

This document contains an overview of typical exam questions for the FEM part of Unit 1 *Numerical Modeling of Construction Materials* of the module CIEM1110. Percentages indicate the work load, where 100% would be the size of a complete exam. The level of difficulty is representative for what you can expect in the actual exam. This collection is not exhaustive in the range of topics that may be covered in the exam.

Questions with solutions

- [5%] 1. (a) Expand the B-matrix for a 4-node element in two-dimensional elasticity in terms of shape functions N_1 to N_4 .
- [5%] (b) Show the role of the Jacobian in the construction of the B-matrix for isoparametric elements.
- [5%] (c) When evaluating the stiffness matrix, where does the term $\det(J)$ appear in the formulation?
- [5%] (d) Explain why the term $\det(J)$ is needed.

Note that the questions do not require an explicit expression of the shape functions.

2. A researcher is investigating the mass diffusion behavior of a new type of material and opts for performing a diffusion FE simulation with backward Euler time integration. However, the size and number of simulations to be performed start to create a computational bottleneck.
- [5%] (a) The researcher decides to switch to a **forward Euler** scheme. For the same model and time step size, how would this choice impact execution time, model accuracy and numerical stability?
- [5%] (b) Another way to accelerate the simulations is to increase time step size while sacrificing as least as possible the accuracy of the scheme. With this in mind, what other time integrator could be recommended and why?
- [25%] 3. Starting from the following pseudocode for computing the element stiffness matrix of a general isoparametric element:

```
1
2     function get_element_stiffness (elem)
3         k_ele = 0.0;
4
5         % your code should come
6
7         % between these lines
8
9         return k_ele;
10
11     end function
12
13
```

Use the coding elements below to complete the function:

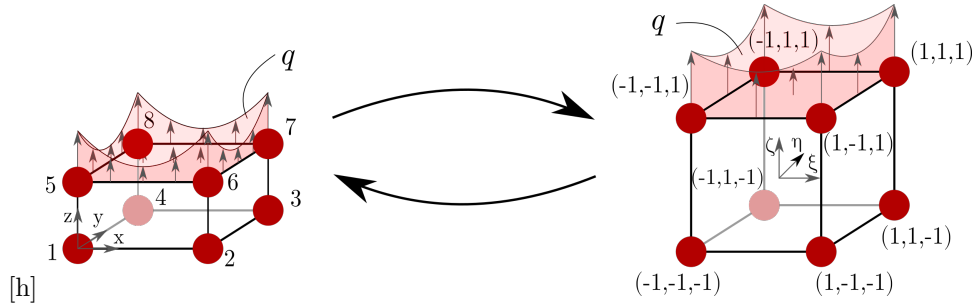
- `for ip = 1..nip`
- `end for`
- `get_node_coordinates (arg)`
- `get_B_matrix (arg)`
- `get_ip_weight (arg)`
- `get_nodes_for_elem (arg)`
- `get_jacobian_at_ip (arg1, arg2)`
- `get_shapegrads_at_ip (arg)`
- `get_D_matrix ()`

Note that some functions have arguments. When writing your answer, clearly indicate which arguments are passed to each function. Assume all functions return a single variable to which you can assign a name

of your choice. You can then use these new variables as arguments for subsequent function calls. Make sure to use all of the above elements when writing your code, adding more lines with basic mathematical operations where necessary. You can also make use of the following operators:

- `matmul(A,b)`: matrix/vector product
- `matmul(A,B)`: matrix/matrix product
- `matmul(A,B,C)`: triple matrix product
- `a * B`: scalar product
- `inverse(A)`: matrix inverse
- `transpose(A)`: matrix transpose
- `determinant(A)`: matrix determinant

- [30%] 4. Consider the following 8-node brick element, to which a surface load is applied on the face defined by nodes 5, 6, 7 and 8:



Nodal coordinates in x-y-z space are given by:

Node	x	y	z
1	0.0	0.0	0.0
2	3.0	0.0	0.0
3	3.0	2.0	0.0
4	0.0	2.0	0.0
5	0.0	0.0	1.0
6	3.0	0.0	1.0
7	3.0	2.0	1.0
8	0.0	2.0	1.0

and the DOFs are arranged in the element vector in the order:

$$\mathbf{a}^{(e)} = [u_{x1} \quad u_{y1} \quad u_{z1} \quad \cdots \quad u_{x8} \quad u_{y8} \quad u_{z8}]^T$$

The magnitude of the surface load varies in space and can be described in isoparametric coordinates as:

$$q = 1 + \xi^2 + \eta^2$$

while shape functions can be given by the compact expression:

$$N_i = \frac{1}{8} (1 + \xi_i \xi) (1 + \eta_i \eta) (1 + \zeta_i \zeta)$$

Based on the information given, answer the following:

- **Compute the surface integral related to the load q** to find the equivalent nodal forces acting on the element. Perform the integration **numerically** and give the equivalent load vector computed with 1x1 Gauss integration. **Clearly show all steps taken**
- How can this integral be evaluated exactly with numerical integration? **Specify the number of integration points** that is needed and **show the procedure for performing the numerical integration** (you do not need to work out the math to arrive)

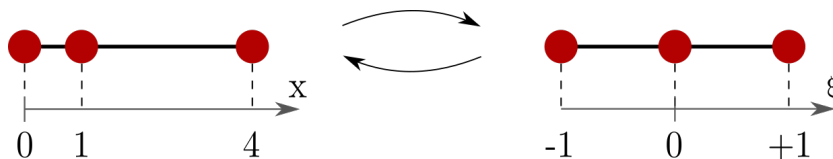
For integration points and weights, refer to the following definition of 1D Gauss integration:

# points	location(s)	weight(s)
1	0.0	2
2	$\pm \frac{1}{\sqrt{3}}$	1
3	$\pm \sqrt{\frac{3}{5}}$	$\frac{5}{9}$
	0	$\frac{8}{9}$

- [25%] 5. Consider a 3-node line element for a bar problem with shape functions defined in the natural coordinate frame as:

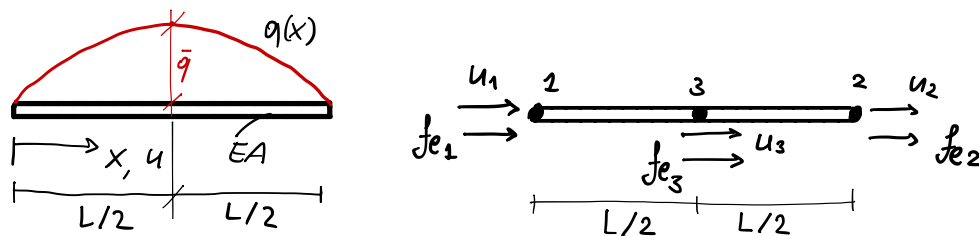
$$N_1 = \frac{1}{2}\xi(\xi - 1) \quad N_2 = 1 - \xi^2 \quad N_3 = \frac{1}{2}\xi(\xi + 1)$$

The nodes of the element are positioned at $x_1 = 0$, $x_2 = 1$ and $x_3 = 4$, as shown in the figure below.



Demonstrate that this element can represent infinite strain inside the element with finite nodal displacements.¹

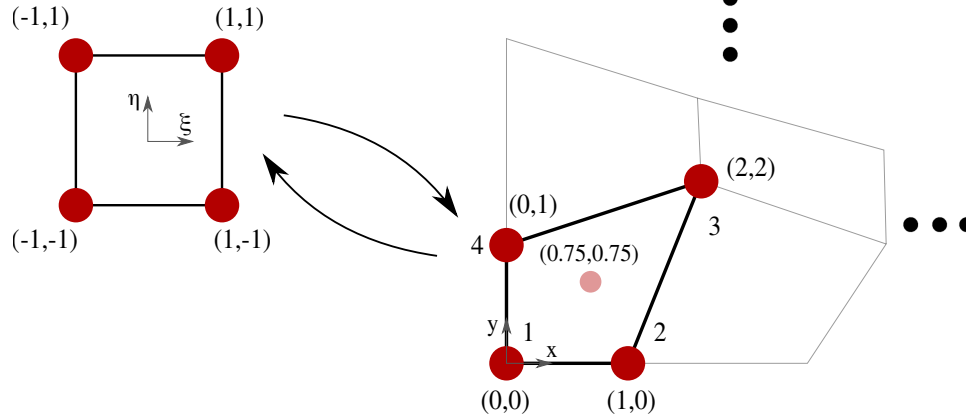
- [35%] 6. Derive the expression of the vector of nodal equivalent forces corresponding to the parabolic distributed load $q(x)$ for the 3-node bar element depicted below starting from the differential equation of the bar. Use a 1- and 2-point quadrature rules in $[-1; 1]$ (location $\pm 1/\sqrt{3}$ and weights equal to 1 for the two-point rule).



¹This question has been asked in an online open book exam. For a closed-book written exam, the question would likely be broken down in smaller steps

Questions without solutions

1. An equilibrium FEM problem is solved with a mesh of distorted Q4 elements, some of which can be seen in the figure below.



The system is solved and a global DOF vector $\mathbf{a}$ is computed. From this global vector, the nodal displacements of the element highlighted in the figure can be extracted:

$$\mathbf{a}^{(e)} = [0 \quad 0 \quad 0.2 \quad 0 \quad 0.4 \quad 0.1 \quad 0 \quad 0.3]^T$$

where DOFs are ordered as $\mathbf{a}^{(e)} = [a_{x1} \quad a_{y1} \quad \cdots \quad a_{x4} \quad a_{y4}]$. The shape functions for this element can be written in the parametric system $\xi - \eta$ as:

$$N_i = \frac{1}{4} (1 + \xi_i \xi) (1 + \eta_i \eta)$$

and the two coordinate systems are related through the Jacobian matrix and its inverse:

$$\mathbf{J} = \begin{bmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial y}{\partial \xi} \\ \frac{\partial x}{\partial \eta} & \frac{\partial y}{\partial \eta} \end{bmatrix} \quad \mathbf{J}^{-1} = \frac{1}{\det \mathbf{J}} \begin{bmatrix} \frac{\partial y}{\partial \eta} & -\frac{\partial y}{\partial \xi} \\ -\frac{\partial x}{\partial \eta} & \frac{\partial x}{\partial \xi} \end{bmatrix}$$

For this problem, the material is modeled as linear-elastic with stiffness matrix given by:

$$\mathbf{D} = \begin{bmatrix} 1000 & 0 & 0 \\ 0 & 1000 & 0 \\ 0 & 0 & 500 \end{bmatrix}$$

- [10%] (a) Using isoparametric mapping, prove that the centroid of the element in $\xi - \eta$ space corresponds to the centroid of the distorted element in physical $x - y$ space (shown in light red in the figure)
- [10%] (b) Describe the procedure to compute the stress vector $\boldsymbol{\sigma}$ at an arbitrary location (ξ, η) inside the element. Employ the isoparametric mapping formalism and for now assume general values for node coordinates, $\mathbf{a}^{(e)}$ and $\mathbf{D}$.
- [20%] (c) Use the procedure you just described to compute the value of the horizontal stress σ_{xx} at point $(0.75, 0.75)$ in physical space. You can simplify your calculations by taking advantage of the zero entries in the values given above.
2. The following pseudo-code snippets and questions relate to coding aspects of the Finite Element Method. Provide a short textual answer to each of them (do not write any code).

- [5%] (a) Part of a loop for computing $\mathbf{K}^{(e)}$ can be seen below:

```

1 # ...
2
3 elmat = 0
4
5 for each integration point:
6     B = compute_B_matrix (dN_dx)
7     D = compute_D_matrix (youngs_modulus, poisson_ratio)
8     thickness = get_thickness()
9
10    elmat += transpose(B) * D * B * thickness
11
12 # ...

```

This code would not integrate a correct stiffness matrix. What is missing from it?

- [5%] (b) Consider the following routine that implements the main loop of a FE solver:

```

1 # ...
2
3 K = 0
4 f = 0
5
6 for each element:
7     K += element_stiffness (element)
8     f += element_bodyforces (element)
9
10 f += point_loads
11
12 solution = invert(K) * f
13
14 # ...

```

This code would not compute a valid solution. What step is missing?

- [5%] 3. (a) With reference to the three-point Newton-Cotes integration rule (NC3), derive the missing information (?) in the table below.

	location ξ_i	weight w_i
1	?	1/3
2	?	?
3	?	?

- [5%] (b) Describe the procedure to perform numerical integration of a function in a generic one-dimensional domain.

- [5%] (c) Integrate $I = \int_1^7 \frac{1}{x} dx$ using NC3

- [30%] 4. Consider the one-dimensional equation of heat conduction with unit conductivity:

$$\frac{d^2\phi}{dx^2} + Q = 0 \quad \text{for } 0 \leq x \leq L,$$

in which

$$Q = \begin{cases} 1 & 0 \leq x \leq L/2 \\ 0 & L/2 \leq x \leq L \end{cases}$$

and $\phi = 0$ at $x = 0$ and $x = L$.

- (a) Derive the weak form at element level.
- (b) Derive the discrete weak form at element level.
- (c) Determine the value of ϕ at $x = L/2$ using a two-element discretization.

Note:

- To apply the boundary conditions $\phi = 0$ strike out corresponding rows and columns in the stiffness matrix. This should generate a 1×1 stiffness matrix.
- Consider a unit cross section.